

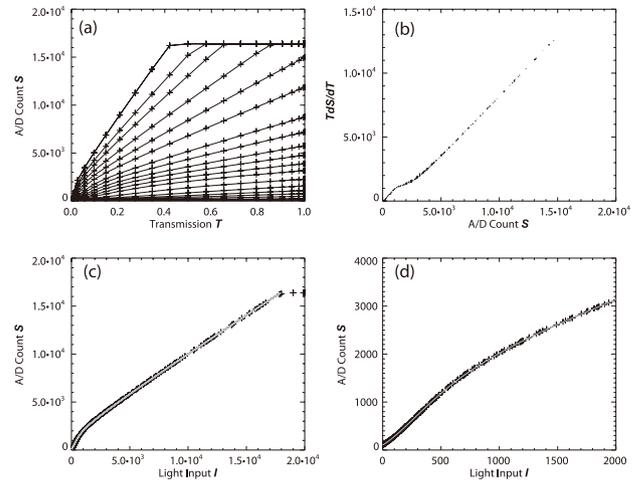
# Practical Method to Derive Non-Linear Response Functions of Cameras for Scientific Imaging

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We developed a practical method to derive response functions which convert the amount of incident light to the A/D counts of cameras for scientific imaging [1]. Some cameras do show non-linear responses, and we have to know them to carry out photometric analysis with the data taken by such cameras. We applied this method for an InGaAs near-infrared camera, XEVA-CL-640 (XENICS), and succeeded to derive a response function, even though it was complicated non-linear one. In principle, such response functions can be derived from the output A/D counts,  $S$ , measured at various incident light levels,  $I$ , which are accurately controlled over the whole dynamic range. However, it is not easy to actually do such measurements with high accuracy. Then we developed a new practical method to derive non-linear response functions. In this method, we need a mechanism to accurately control the amount of incident light into cameras just within a limited dynamic range and at a limited number of steps (relative light level  $T$ , which may be exposure time, transparency, etc.). A variable brightness light source (brightness  $B$ ), which supplies the incident light into cameras, is also necessary, but we do not need to know its accurate brightness.

Figure 1(a) shows the raw results measured under such conditions; output A/D values,  $S$ , are measured at several  $T$ 's under various unknown  $B$ 's (the brightness of the incident light,  $I$ , is written as  $I = BT$ ). It seems that without knowing  $B$ 's, it is difficult to derive the relation between  $I$  and  $S$  from the results shown in Figure 1(a). However, we can derive  $IdS/dI$ , because the relation  $dI = BdT$  based on  $I = BT$  brings  $dS/dT = BdS/dI$ , and this means  $TdS/dT = TBdS/dI = IdS/dI$ . The value  $TdS/dT$  can be derived from the known values,  $T$  and  $S$ , and therefore, without knowing  $B$ , we can derive a unique relation between  $T$  and  $TdS/dT (= IdS/dI)$  as shown in Figure 1(b). The relation seen in Figure 1(b) can be converted to the relation between  $I$  and  $S$  through the numerical integration. Figure 1(c) shows the derived relation between  $I$  and  $S$ , namely the response function of the camera. Obviously the function is non-linear. Figure 1(d) shows a close-up of the low-light level portion of Figure 1(c), and we can find a complex non-linear behavior.

We are using a XEVA camera for the polarimetry of the infrared solar light, which requires high accuracy measurements. Compensation of the non-linearity based on the derived function works well, and we have quantitatively high-quality observational data.



**Figure 1:** (a) Measured A/D counts  $S$  at various values  $T$  are shown with plus signs. Each line represents the measurements carried out under the same brightness  $B$  of the light source. (b) Relation between the measured A/D count,  $S$ , and the  $TdS/dT$  value. All the measured points are on a unique curve, regardless of the values of  $B$ . (c) Calculated non-linear response function between the amount of light input,  $I$ , and the output A/D count,  $S$ , is shown with a solid grey line. The measured points shown in Figure 1(a) are also plotted with plus signs. (d) Enlargement of the low- $I$  range of panel (c).

## Reference

- [1] Hanaoka, Y., Suzuki, I., Sakurai, T.: 2011, *App. Opt.*, **50**, 2401-2407.